# Planning and Control of Marine Floats in the Presence of Dynamic, Uncertain Currents

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#### **Abstract**

We address the control of a vertically profiling float using ocean-model-based predictions of future currents. While these problems are in reality continuous control problems, we solve them by searching a discrete space of future actions. Additionally, while the environment is a continuous space, the ocean model we use is a discrete cell-based model. We show that even with an imperfect model of ocean currents, planning in the ocean current model can significantly improve results for a specific problem of controlling a vertically profiling float when a trade-off between remaining at the same location as a virtual mooring and collecting more data with more profiles is available. We also present anecdotal data from an April 2015 deployment of EM-APEX floats.

## Introduction

The study of ocean dynamics is an important problem with many ramifications including environment and climate, food production, defense, and leisure. There are a variety of different techniques currently being used to monitor and measure ocean conditions such as currents, salinity, and temperature. Recent advances in robotic marine vehicles such as floats, gliders, and autonomous underwater vehicles (AUV) provide a plethora of new tools and techniques for ocean measurement. Another important way that scientists are able to collect measurements is by using moored buoys. This allows scientists to collect data at a fixed location over time. However, physically mooring a buoy is a significant financial investment and the mooring is only able to collect data at a fixed location.

As an alternative, a *virtual mooring* has been proposed in which a dynamically controlled vehicle uses a control policy in order to maintain its position. Specifically, one proposal is to deploy a vertical profiling float to the location of desired data collection and using predictive ocean models to plan a control sequence for changing depths that best keeps the float near the same location using the ocean currents. This method has multiple benefits over using a float at a physical mooring. First, the float could be retrieved and redeployed when desired. Second, there is more flexibility in that the float could be programmed to track a moving target

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Asset	Control	Speed	Longevity	Cost
Floater	None	None	Weeks	\$100's
Vertical Profiling Float	Vertical	∼0.1 m/s	Years	\$10K's
Seaglider	Horizontal	~0.5 m/s	Months	\$50's - \$100'sK
AUV	Horizontal & Vertical	$\sim$ 2.5 m/s	1 Day - Weeks	\$100K - \$M

Table 1: Characteristics and costs for different families of marine vehicles.

or to drift to facilitate deployment or retrieval. Third, the deployment would be less expensive than building a physical anchor location.

Although using an AUV would provide better control to remain at a fixed location, more capable vehicles are more expensive. Table 1 shows approximate costs for families of marine vehicles (Woods Hole Oceanographic Institution; Sanford et al. 2005; Eriksen et al. 2001; YSI Systems; OceanServer Technology, Inc.; Bluefin Robotics Corporation; Kongsberg Mairtime AS).

We believe that deploying a vertical profiling float is a cost effective alternative to using physical moorings or AUVs by using predictive ocean models to generate a control sequence that allows the float to act as close as possible to a virtual mooring considering the ocean currents and that when flexibility is available, a trade-off can be made to collect more data profiles and float away from the mooring location.

A prior version of this float planning scheme was deployed in April 2015 to control two Electromagnetic Autonomous Profiling Explorer (EM-APEX) (Sanford et al. 2005) floats. In this deployment, an incoming weather front made the ocean model a poor predictor of ocean currents and therefore could only validate the negative hypothesis that when the ocean model is not a good predictor that the planning-based control will not yield good results.

#### **Problem Definition**

This experiment generates a control sequence for a vertical profiling float to make it act as a virtual mooring. Given a start location, a goal location, a mission duration, and a planning model of ocean currents, the goal is to produce an optimal sequence for a float with a particular diving and surfacing speed in the planning model and to verify that it does well in the nature model, based on a desired objective function.

The start location represents the drop-off location of the float and the goal location represents the location of the virtual mooring, which is equivalent to the desired data collection site. The mission duration is the length of time for which a control sequence will be generated. In an ideal situation, a data measurement would be collected at all times and at all depths at the same latitudinal and longitudinal location. However, given a single float, a trade-off has to be made between profiling across all depths and drifting away from the mooring location. Therefore, the objective function should take this into account and make a compromise between collecting data at different depths or staying close to the desired location. The ocean models contain current information at varying depths, which is used to determine where the float will move during the mission duration. Since predictive ocean models cannot perfectly forecast the ocean currents, the planning model represents this imperfect knowledge and the nature model represents the actual ocean currents. In this way, it is possible to approximate a scenario of generating a control sequence in an ocean model and executing it in the ocean.

## **Experimental Inputs**

For this experiment, the vertical profiling float was given a vertical speed of 0.12 m/s taken as the speed of the operational EM-APEX floats used in prior deployments. The maximum profiling depth was chosen to be 500 m. The mission duration was set to be one day.

The start location and the goal location were (latitude, longitude) locations at the surface of the ocean. They were set to be the same location so that it represents a float that is placed at the location of desired data collection. In particular, nine different start/goal locations in the Monterey Bay Area were chosen for this experiment. These locations are shown in Fig. 1 and table 2.

**latitude:** 36.872217 36.072217 35.272217 **longitude:** -123.734853 -123.134853 -122.534853

Table 2: The three latitudes and longitudes that make up the nine starting/goal locations used as experimental inputs.

The ocean model used for this experiment was the Regional Ocean Modeling System (ROMS) (Chao et al. 2009; Li et al. 2006; Farrara et al. 2015), a discrete, cell-based model. For our experiments we used a ROMS California coast configuration with a grid size of approximately 3 km in the latitudinal and longitudinal directions, 1 hour in the time dimension over 72 hours, and fourteen depths ranging from 0 to 1000 m in non-uniform intervals. The ocean currents vary with latitudinal and longitudinal direction as well as depth. The deeper currents tend to be more consistent and slower, whereas the surface currents are more variable and



Figure 1: The nine starting/goal locations used as experimental inputs.

often have a higher velocity.

In order to approximate a scenario of planning with the predicted ocean model and executing the control sequence in the ocean, two different models were used. Both models are ROMS models, thus both models are discrete and cellbased, and computations are done in the some manner. Using the standard practice in ocean modeling, the planning model uses information from ten days before the desired day of execution without HF radar assimilation. The nature model incorporates the HF radar assimilation and represents the conditions of the ocean on the desired day of execution and is the best model of the ocean on that day. Table 3 shows the different inputs to ROMS for the planning and nature models. By using the two different models with different predictive knowledge, it is possible to simulate using a predictive model for planning and executing that plan in an actual deployment. The planning model is used to plan exactly the way it would be in a deployment and the nature model is used when replicating the path as a simulation for an ocean deployment. The models for this experiment were generated for April 17, 2015.

Figure 2 demonstrates how the zonal and meridional currents vary between the two different models. The zonal currents are in the west-east direction and the meridional currents are in the north-south direction. The currents are shown for location (34.66°lat, 235.68°lon) at the surface over 72 hours.

The objective function was designed to trade-off profiling and remaining close to the mooring location and to favor one or the other by changing the relative weights between the terms. The equation for the objective function is

$$\sum_{n} \sum_{d} (w_T T_d + w_D D_d)$$

where n are the nodes in the path, d are the depth choices,

	Planning Models	Nature Model
Archiving, Validation and	X	X
Interpretation of Satellite		
Oceanographic (AVISO)		
sea surface height data		
Advanced Very High Resolution	X	X
Radiometer (AVHRR) sea		
surface temperatures		
Moderate Resolution Infrared	X	X
Spectroradiometer (MODIS)		
sea surface temperatures		
GOES satellite sea surface	X	X
temperatures		
High Frequency (HF)		X
radar surface current data		
Monterey Bay Aquarium	X	X
Research Institute (MBARI)		
M1 mooring vertical profiles		
of temperature and salinity		
Ship sea surface temperatures	X	X
Number of days advanced	10	1
prediction		

Table 3: ROMS inputs for the planning and nature models.

and  $w_T$  and  $w_D$  are weighting terms.  $T_d$  is the number of seconds since the last time the path was at depth d divided by 1000.  $D_d$  is the distance in kilometers that the path was from the goal location the last time the path was at depth d.

In other words, at each time step the most recent node at the surface and at the profiling depth are found and  $(w_TT_d+w_DD_d)$  is added to the objective function. Since  $T_d$  can be used as a proxy for determining the time since the last profile, a smaller  $w_T$  to  $w_D$  ratio favors control sequences that keep the float closer to the desired data collection site, whereas a larger  $w_T$  to  $w_D$  ratio favors control sequences that have more profiles.

## Algorithm

Even though, in reality, the problem space is continuous, in order to make the search tractable the future actions of the float are determined in a discrete manner. At each time step, the possible actions are to move to the surface or to move to the selected maximum profiling depth. In other words, if the float is at the surface it can either stay at the surface or move to the profiling depth and if the float is at the profiling depth it can remain there or return to the surface. If the float stays at a depth, the duration is equivalent to the amount of time required to move between the surface and the maximum profiling depth. This means that each time step is equal in length. One profile is defined to be one trip down and up again.

The current information that was used to calculate the motion of the float was determined based on the float's latitudinal and longitudinal location, its depth, and the time. If remaining at the same depth, the data from the model cell at the closest latitude, longitude location and previous hour index of the beginning of the time step was used. If moving

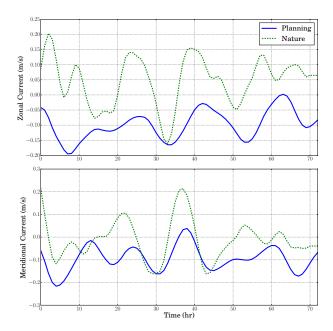


Figure 2: Velocities at the surface of location (34.66°lat, 235.68°lon) over 72 hours for the planning and natures models.

through depths, the time to move through the discrete depths that are available in the ROMS model is calculated such that a new latitude, longitude location and time is calculated for the arrival at each depth. It is that data that is used to choose the cell from which to extract the current information in the same manner as when staying at the same depth: the closest latitude, longitude cell is chosen and the time index is for the previous hour. Currently, no interpolation is being applied between the grid points, neither in location nor in time.

The algorithm used to search for the control sequence is an A\* algorithm with a zero heuristic estimator. A path is considered finished once the mission duration has been reached. Once a path has reached the length of the mission duration, the score is saved as the best path score and the queue is flushed to finish all remaining paths while they have a score that is less than the best finished path so far. If a finished path has a score that is better than the best path, that score becomes the best path score. Since the queue is completed to expand all paths with a lower score after finding the first complete path, this algorithm is optimal.

The following pseudocode in Algorithm 1 summarizes the execution of the algorithm.

#### **Experimental Procedure**

At each location, the algorithm described above was run using the planning model with a ratio of  $w_T$  to  $w_D$  ranging from 0.4 to 20.0 in steps of 0.4. The maximum number of profiles that can be achieved in the chosen mission length is 10 so there are 20 points at which a decision must be made and since there are two possible choices to make at each point, this results in  $2^{20}$  possible control sequences. Two specific control sequences were also run on the plan-

## Algorithm 1 Batch Planning A\* Algorithm

```
Q \leftarrow start location
while Q not empty do
    curPath \leftarrow lowest objective score path in Q
    newPath1 \leftarrow curPath + node at surface
   newPath2 \leftarrow curPath + node at profiling depth
   if either newPath duration > mission duration then
        bestPath \leftarrow curPath
        bestScore \leftarrow curPath \text{ score}
        break
    end if
    Q.push(newPath1)
    Q.push(newPath2)
end while
while Q not empty do
                                       \triangleright Flush the rest of Q
    curPath \leftarrow lowest objective score path in Q
    if curPath score > bestScore then
        break
    end if
   newPath1 \leftarrow curPath + node at surface
   newPath2 \leftarrow curPath + node at profiling depth
    if either newPath duration > mission duration then
        bestPath \leftarrow curPath
        bestScore \leftarrow curPath \text{ score}
    else
        Q.push(newPath1)
        Q.push(newPath2)
    end if
end while
```

ning model. The first required the float to remain at the surface and the second required the float to continuously profile. Once the optimal control sequences were determined in the planning model, these sequences are then executed in the nature model. The surface and continuous profiling sequences were also run in the nature model. In order to analyze whether planning for the control sequence in the planning model improves the goal of remaining close to the virtual mooring location, a baseline control sequence needed to be chosen as a comparison. As our baseline we chose evenly spaced profiles at each available number of profile choice. Specifically, since 10 full profiles can fit within the mission length, therefore the baseline sequences were 1 through 9 evenly spaced profiles. Remaining and the surface (0 profiles) and full profiling (10 profiles) were calculated separately, as described previously.

## **Empirical Evaluation in Simulation**

Each location and weight combination results in a control sequence for the float. This means that for each location, fifty runs with different trade-offs between profiling and remaining near the goal location were executed. However, due to the nature of the values of the ratio of the weights that are applied to the objective function, many control sequences are identical among similar weights. Furthermore, due to the discrete selection of weights, not all numbers of possible profiles are generated at each location.

As an example, Fig. 3 shows the path that was generated using the optimal path at location (35.272217°lat, -123.734853°lon) and weight ratio 2.4 in the planning model and the nature model. The blue path is the path in the planning model and the red path is in the nature model.

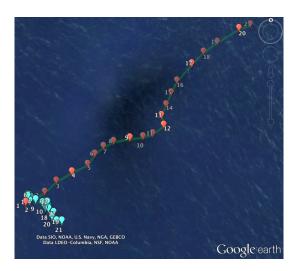


Figure 3: Optimal path at location (35.272217°lat, -123.734853°lon) and weight ratio 2.4 in the planning model (blue) and the nature model (red).

Figure 4 shows the control sequence for that path (top) as well as the distance (middle) and sum of distances (bottom) at each time step. In other words, the middle graph shows the instantaneous distance from the goal and the bottom graph shows the instantaneous sum of the distances so far from the goal. This particular example shows that in the planning model, the path results in 5 full profiles, ends at a distance of approximately 15 km from the goal location, and the sum of the distances from the goal location at each step in the path ends at almost 160 km. In the nature model, on the other hand, the distance from the goal at the end of the path is now approximately 2 km and the sum of the distances is approximately 17 km.

In this particular example, the execution in the nature model resulted in an end distance and sum of distances smaller than those in the planning model. However, this may not always be the case. It is expected that sometimes the currents in the nature run will be more favorable and sometimes they will be less favorable to keeping the vertical profiling float near its goal location, but that on average the difference will be close to zero. What this would indicate is that the planning model is a good predictor for the nature model and thus provides effective planning information.

Let  $D_{End}$  be the difference between the distance from the goal at the end of the mission in the planning run and the nature run in kilometers. A positive difference means that the distance in the nature run was larger than that of the planning run.

Let  $D_{Sum}$  be the difference between the sum of the distance from the goal at each node in the path in the planning run and the nature run in kilometers. A positive difference

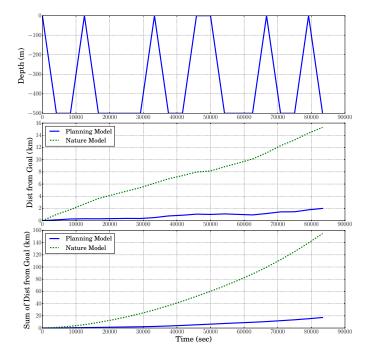


Figure 4: The control sequence (top), end distance from the goal (middle), and sum of distances from the goal (bottom) for the example path at location (35.272217°lat, -123.734853°lon) and weight ratio 2.4 in the planning model and the nature model.

means that the sum of the distances in the nature run was larger than that of the planning run.

These results show that the previously held expectation does not hold for our sample size. This indicates that the planning model lacks information and is not a perfect predictor, even on average. This is further confirmed by observing the correlation coefficient between the zonal currents in the planning and nature models as well as the meridional currents in the two models. The correlation coefficient for the two currents in the planning and nature models at the surface depth and first time index was calculated using the cells in the search region around the example starting location. Specifically, the velocities for all the surface cells in the search region were placed in the following vectors,  $Zonal_{plan}$ ,  $Meridional_{plan}$ ,  $Zonal_{nature}$ , Meridional<sub>nature</sub> according to the velocity direction and model. Using these vectors, the meridional correlation coefficient,  $\rho_{Meridional}$  and the zonal correlation coefficient,  $\rho_{Zonal}$  were calculated using the equations

$$\begin{split} \rho_{Meridional} &= \frac{\text{Cov}(Meridional_{plan}, Meridional_{nature})}{\sigma_{Meridional_{plan}}\sigma_{Meridional_{nature}}} \\ \rho_{Zonal} &= \frac{\text{Cov}(Zonal_{plan}, Zonal_{nature})}{\sigma_{Zonal_{plan}}\sigma_{Zonal_{nature}}} \end{split}$$

where Cov is the covariance function and  $\sigma_{Meridional_{plan}}$ ,  $\sigma_{Meridional_{nature}}$ ,  $\sigma_{Zonal_{plan}}$ , and  $\sigma_{Zonal_{nature}}$  are the standard deviations of the referenced vector. These coefficients are shown in the table below.

Those small, positive correlation coefficients substantiate the claim that the planning model provides some predictive knowledge, but it far from a perfect predictor for the nature model.

The following graph, Fig. 5, shows the results for all of the weights at the same location used in the previous example: (35.272217°lat, -123.734853°lon). To properly convey the results in terms of the objective function, it would be best to show the distance from the goal and use the time since the float was at a particular depth. However, this time value is difficult to conceptualize in a concrete manner, and since it is a proxy for the number of profiles that are achieved, it was decided to display the results in terms of the number of profiles instead of the time term in the the objective function. The open circles are the results in the planning model and are labeled by the weighting ratio  $w_T/w_D$  that resulted in that result. The open squares show the results of remaining at the surface or purely profiling in the planning model. The closed circles are the results of using the control sequences generated in the planning model in the nature model and are also labeled with the weighting ratio that was used in planning the sequence. The closed squares show the results of the reference control sequence of evenly spaced profiles in the nature model.

This particular example demonstrates how the span and discrete selection of the weighting ratio does not result in all possible number of profiles and that multiple weighting ratios result in the same control sequence. This graph also shows that for this location, for all weights the distance in the nature model was greater than that in the planning model and that the baseline control sequence always did worse than the planned sequence in the nature model.

Let  $D_{RefEnd}$  be the difference between the distance from the goal at the end of the mission in the nature model with the reference control sequence and the planned control sequence. A positive difference means that the distance using the reference control sequence was larger than that of the planned sequence.

Let  $D_{RefSum}$  be the difference between the sum of the distance from the goal at each node in the path in the nature model with the reference control sequence and the planned control sequence. A positive difference means that the distance using the reference control sequence was larger than that of the planned sequence.

The following tables, Table 4 and Table 5, summarize the results in terms of  $D_{RefEnd}$  and  $D_{RefSum}$  over all locations and weighting ratios. Paths from control sequences that resulted in the same number of profiles were compared to each other. Since not all weighting ratios achieve all possible number of profiles, there are a different number of paths that are compared for the different profile numbers. The column headed "Num" shows this number. What these metrics

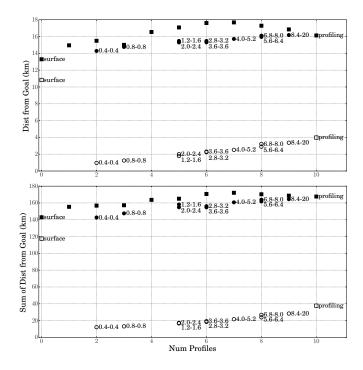


Figure 5: Distance from the goal location, sum of distance from the goal location, and number of profiles for each weighting ratio at location (35.272217°lat, -123.734853°lon) in the planning and the nature models. The open circles represent the results in the planning model, the closed circles represent the results in the nature model, and the squares represent the results of the baseline sequences.

demonstrate are whether, when there is flexibility as to when the float will profile, planning for the timing of the profiles in an ocean model provides for better virtual mooring than evenly spacing out the profiles, which is like doing a random plan.

Profiles	Num	Avg $D_{RefEnd}$	Stdev $D_{RefEnd}$
1	7	0.62	8.70
2	4	2.70	3.62
3	7	-5.87	8.62
4	7	2.72	4.63
5	12	3.35	2.44
6	14	3.14	2.51
7	16	1.21	2.13
8	19	0.56	1.60
9	14	-0.41	1.51

Table 4: Results with respect to the baselines over all 9 locations and 50 weighting ratios comparing paths with the same number of profiles with respect to the end distance of the path from the goal location. A positive difference indicates that planning does better than the baseline. Duplicate paths from different weighting ratios are excluded resulting in less than  $9 \times 50 = 450$  paths compared.

Profiles	Num	Avg $D_{RefSum}$	Stdev $D_{RefSum}$
1	7	13.38	87.88
2	4	31.57	53.71
3	7	-47.83	81.84
4	7	23.50	40.12
5	12	24.27	20.11
6	14	20.12	23.28
7	16	1.67	21.19
8	19	1.57	14.12
9	14	-0.60	8.96

Table 5: Results with respect to the baselines over all 9 locations and 50 weighting ratios comparing paths with the same number of profiles with respect to the sum of the distance of the path from the goal location. A positive difference indicates that planning does better than the baseline. Duplicate paths from different weighting ratios are excluded resulting in less than  $9 \times 50 = 450$  paths compared.

The values in these tables indicate that, in general, planning is beneficial for remaining near the goal location instead of using evenly spaced profiles, as was expected from the previous analysis of the correlation coefficients. Looking at the results for 3 and 9 profiles, the distances are negative, meaning that planning did worse than the baseline for these two cases. One possibility is that more data needs to be collected, possibly over different locations and different days, in order to smooth out the noise and get a better representation of the problem, and that on this particular day, the nature model had particular characteristics that were not captured in the planning model for those paths. More data collection would need to be done to analyze this anomaly further.

### **Empirical Results in Deployment**

A prior version of this software was deployed to control EM-APEX floats during an April 2015 deployment in support of an AirSWOT (Jet Propulsion Laboratory a; b) field experiment in the coast off of Monterey Bay, California. In this field experiment, the goal was to keep EM-APEX floats near features of interest identified manually by scientists. The overall AirSWOT deployment goals are representative of the intended scientific use case for these planning tools.

The overall AirSWOT deployment was to test out an Airborne science instrument by providing corroborative data over interesting science features using in-situ instrumentation (floats, ships) and remote sensing data (from overflying spacecraft). The AirSWOT instruments were scheduled to fly in a coverage pattern over specific areas chosen to overlap satellite overflights.

Three EM-APEX floats were to be deployed to be near satellite overflights and airborne overflights. The float planning tool was used to evaluate potential deployment locations by predicting the projected drift path of the floats.

Figure 6 shows the variability of the expected float drift based on the deployment location. The blue paddle indicates the start location and the green path shows where the float was projected to drift over time.

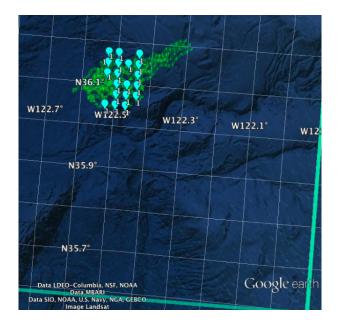


Figure 6: Expected float drift based on starting location. The blue paddle indicates the starting location and the green paths shows the drift.

Sites for each of the three float deployments were screened for projected stability and hand selected by the experiment team.

Additionally, two of the three EM-APEX floats were allowed to be controlled dynamically from shore by an earlier version of the float planning software. This prior float planning software received the satellite phone updated location each time the target float surfaced. Because of connectivity issues, the float planning software could not receive this data rapidly enough to generate a new plan for transmission to the float during this surface cycle as the float was only on the surface approximately 30 minutes each cycle. Instead the planner could only assert a plan with a 1 surface cycle lag. Therefore the plan communicated to the float to be executed after surface cycle n was only based on the actual position from cycle n-1 plus the projected drift from cycle n-1 to cycle n.

The EM-APEX float tracks planned and executed are shown for floats 6665 and 6667 in Fig. 7. The yellow point indicates the start location of the float. The actual location of the float at each surfacing is shown in blue with the arrows indicating the direction. The red points show where, at each step of re-planning, the float was predicted to travel. Since the re-planning was performed two cycles ahead, two surfacing locations are displayed. As shown, the expected control for neither of the floats performed very well.

This poor performance is not surprising as the current velocities in the ROMS model in the area near both floats was not very accurate, as can be seen in Fig. 8 and Fig. 9. Because EM-APEX is designed to get velocity data, it provides a good opportunity to compare collected data to the ROMS model. The plots show the zonal and meridional currents that were used in the ROMS model at each depth traversed in the

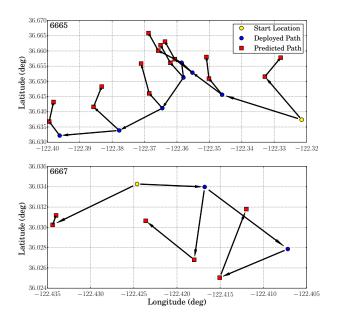


Figure 7: The deployed path and predicted path at each replanned step in the deployed path for floats 6665 and 6667.

path as well as the currents that were collected by the float at those same depths, when that data was available. The vertical lines indicate the boundary between profiles so that the line indicates when the path is at the surface of the ocean.

The poor correlation between the ROMS and the float collected velocities is most likely due to the front that was coming in during the deployment that even caused the deployment to be cut short.

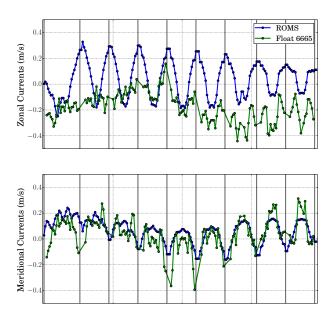
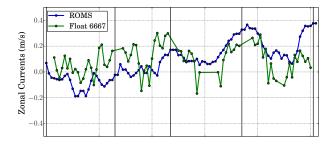


Figure 8: Zonal and Meridional currents found along the path for float 6665 in the ROMS model and actually experienced in the deployment.



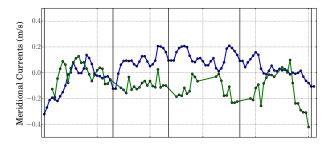


Figure 9: Zonal and Meridional currents found along the path for float 6667 in the ROMS model and actually experienced in the deployment.

The results from the April 2015 deployment reinforce the thesis of this paper. In cases where the current model provides significant information, the model information can be used improve to float control. In cases where the model provides no or bad information performance will be poor and even in some cases worse than open loop algorithms such as constant profiling.

#### **Related Work**

Path planning for underwater vehicles has been widely studied; however, there has been relatively little work in float planning. A notable exception is (Dahl et al. 2011) which examined the problem of optimizing coverage across the oceans for a large number of floats, but only considered a constant depth and a greedy algorithm. Much more research has been done on glider planning, where there is some control for choosing a direction of motion, but it is less than the current velocity. (Thompson et al. 2010) also uses the ROMS model, but calculates reachability envelopes using wavefront propagation for glider path planning. The work in (Eriksen et al. 2001) describes Seaglider, a glider that is manually controlled from the shore, and is sometimes controlled to maintain position. No ocean model similar to ROMS was used. (Alvarez, Garau, and Caiti 2007) also does not use an ocean model, but instead uses synthetic data with general algorithms to control a set of floats and gliders. Like the work in this paper, (Rao and Williams 2009) uses an A\* graph search algorithm; however, that work assumes that currents change slowly with time and compute the path across many nodes in a single time step, whereas we have many time steps within a single cell. Instead of trying to remain near a specific location, (Pereira et al. 2013) focuses on gliders that are attempting to avoid surfacing in dangerous areas, such as shipping lanes. (Grasso et al. 2010) focuses on

the prediction of the glider location, analyzes the accuracy of the predictive model, and uses a physics based control model. Using an asset with more control, (Cashmore et al. 2014) explores the problem of autonomously maneuvering near a site for inspection using an AUV with probabilistic modeling for uncertainty. Autonomous marine vehicles have even been proposed to explore Titan, a moon in the Saturnian system (Pedersen et al. 2015; ESA/NASA 2009; Stofan et al. 2009).

#### **Future Work**

There are future extensions to further validate the modelbased planning approach to sea asset control. Smoothing, or interpolation, of the grid points in the model could be performed when determining the current velocity at a location and time. Different types of goal locations could be used, such as a line, a grid, or even a moving point. Similarly, the start location could be different from the goal location. The deployment cost and retrieval cost could be incorporated into the overall objective function. The search could include asset selection with an asset cost metric, e.g. the asset could be changed from a float to a glider or an autonomous underwater vehicle to add more flexibility to the control sequence when such an asset is available. Multiple assets of different types could be planned for at once with different goal locations. The algorithm could be changed to be an incomplete or suboptimal algorithm in order to decrease the run time. Another scenario could be to re-plan the control sequence with every surfacing of the asset. This would simulate a scenario in which the most recent, real information about the location of the asset could be used to create a better control sequence during the execution. Finally, we are exploring use of these algorithms in experiment design - in which a range of locations within a specific region of interest are considered and a virtual mooring location is chosen that is expected to be location maintainable.

#### **Conclusions**

Based on these results, it is clear that modeling the ocean for the purpose of planning trajectories is a very difficult problem. We saw that the currents in the planning model and the nature model are weakly, positively correlated, so although the planning model does not perfectly capture the ocean movement in the nature model, it is a useful tool that leads to improved control sequences, as was demonstrated by the results of the planned control sequences compared to the baseline sequences as well as the actual deployment data. This method could also be used to help in the selection of a virtual mooring site in order to find the location where it is least likely that the float will be carried away from the goal location.

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